

Liquid Supply System, Ink Jet Recording Head, Ink Jet
Recording Apparatus and Liquid Filling Method

BACKGROUND OF THE INVENTION

5 Field of the Invention

The present invention relates to an ink jet recording head, an ink jet recording apparatus employing such inkjet recording head, and a liquid supply system suitable for use therein.

10 Related Background Art

Among various recording methods in printers or the like, the ink jet recording method for forming a character or an image on a recording medium by discharging ink from a discharge port (nozzle) is
15 widely employed in recent years because it is a non-impact recording method of low noise level capable of high-density and high-speed recording operation.

An ink jet recording apparatus is generally provided with an ink jet recording head, means for
20 driving a carriage supporting such recording head, means for conveying the recording medium, and control means for controlling these components. An apparatus executing the recording operation under such carriage motion is called serial scan type. On the other hand,
25 an apparatus executing the recording operation by the conveying of the recording medium only, without moving the ink jet recording head is called line type.

In the ink jet recording apparatus of line type, the ink jet recording head is provided with a plurality of nozzles arranged over the entire width of the recording medium.

- 5 The ink jet recording head is provided with energy generating means for generating discharge energy to be given to the ink in the nozzle, in order to discharge therefrom an ink droplet. The energy generating means can be an electromechanical
- 10 converting element such as a piezo element, an electrothermal converting element such as a heat generating resistor, an electromagnetic wave-mechanical converting element or an electromagnetic wave-thermal converting element for converting
- 15 electromagnetic wave such as electric wave or laser light into mechanical vibration or heat. Among these, a method for discharging ink droplet by thermal energy can achieve recording of high resolution because the energy generating means can be arranged
- 20 at a high density. Particularly an ink jet recording head utilizing an electrothermal converting element as the energy generating means can be made compact more easily than a head utilizing the electromechanical converting element, and provides
- 25 advantages of easily achieving high-density configuration and low manufacturing cost, utilizing the IC technology and the micro fabrication

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technology showing remarkable progress and improvement in reliability in the semiconductor area.

In the system of ink supply to the ink jet recording head, there are known so-called integral ink tank system in which an ink tank containing the ink is integrated with the ink jet recording head, so-called separated ink tank system in which the ink tank is separated from the ink jet recording head, so-called tube supply system in which the ink tank and the ink jet recording head are connected by a tube, and so-called pit-in system in which the ink tank and the ink jet recording head are provided separately but the ink jet recording head is moved to the position of the ink tank whenever required and is connected thereto for executing ink supply from the ink tank to the ink jet recording head.

When the capacity of the ink tank is increased in order to reduce the frequency of replacement thereof, the weight thereof increases. This means an increase in the weight of the carriage in the recording apparatus of serial scan type. In consideration of this fact, the ink jet recording apparatus of serial scan type requiring the ink tank of a large capacity for example for outputting a large sized recorded image often employs the tube supply system or the pit-in system. Among these, the tube supply system capable of continuous recording

over a long period is often employed since, in the pit-in system, the recording operation has to be interrupted during the ink supply operation.

In the following the ink supply system of an ink jet recording apparatus of tube supply system will be explained with reference to Fig. 25.

The ink supply system shown in Fig. 25 is provided with a main tank 1204 containing ink therein, a supply unit 1205 on which the main tank 1204 is detachably mounted, and a recording head 1201 connected to the supply unit 1205 through a supply tube 1206.

The supply unit 1205 is provided therein with an ink chamber 1205c, which is open to the air by an air communicating port 1205g at the upper portion and is connected at the bottom portion to the supply tube 1206. On the supply unit 1205, there are fixed a hollow ink supply needle 1205a and a hollow air introducing needle 1205b of which lower ends are positioned in the ink chamber 1205c and higher ends protrude from the upper face of the supply unit 1205. The lower end of the ink supply needle 1205a is positioned lower than that of the air introducing needle 1205b.

The main tank 1204 is provided at the bottom thereof with two connector portions composed for example of rubber stoppers for closing the interior

of the main tank 1204, whereby the ink tank singly
has a hermetically closed structure. The mounting of
the main tank 1204 to the supply unit 1205 is
executed in such a manner that the ink supply needle
5 1205a and the air introducing needle 1205b
respectively penetrate the connector portions and
enter the interior of the main tank 1204. Since the
lower ends of the ink supply needle 1205a and the air
introducing needle 1205b are positioned as explained
10 in the foregoing, the ink in the main tank 1204 is
supplied to the ink chamber 1205c through the ink
supply needle 1205a and the air is introduced into
the main tank 1204 through the air introducing needle
1205b so as to compensate the pressure decrease
15 resulting in the main tank 1204. When the ink is
supplied into the ink chamber 1205c until the lower
end of the air introducing needle 1205a is immersed
in the ink, the ink supply from the main tank 1204 to
the ink chamber 1205c is terminated.

20 The recording head 1201 is provided with a sub
tank 1201b for containing ink of a predetermined
amount, an ink discharge portion 1201g having an
array of plural nozzles for ink discharge, and a flow
path 1201f connecting the sub tank 1201b and the ink
25 discharge portion 1201g. In the ink discharge
portion 1201g, a face having the nozzle apertures is
directed downwards, so that the ink is discharged

downwards. Each nozzle in the ink discharge portion 1201g is provided with the aforementioned energy generating means. The sub tank 1201b is positioned higher than the ink discharge portion 1201g, and the supply tube 1206 is connected to the sub tank 1201b. Between the sub tank 1201b and the flow path 1201f, there is provided a filter 1201c having a fine mesh structure in order to prevent clogging of the nozzle resulting from the entry of fine foreign particles into the ink discharge portion 1201g.

The area of the filter 1201c is so selected that the pressure loss in the ink does not exceed a tolerance value. The pressure loss in the filter 1201c increases as the mesh thereof is finer or the ink flow rate through the filter is higher, but is inversely proportional to the area thereof. Since the pressure loss tends to become higher in the recent recording head of high-speed, multi-nozzle and small recording dots, the area of the filter 1201c is selected as large as possible to suppress the increase in the pressure loss.

Since the nozzle in the ink discharge portion 1201g is open to the air and directed downwards, the interior of the recording head 1201 has to be maintained at a negative pressure relative to the atmospheric pressure in order to prevent ink leakage from the nozzle. On the other hand, an excessively

large negative pressure causes entry of gas into the nozzle, whereby the nozzle becomes incapable of discharging ink. Therefore, in order to maintain a suitable negative pressure in the recording head 1201, 5 the recording head 1201 is so positioned that the nozzle aperture face is higher, by a height H, than the ink liquid level in the ink chamber 1205c thereby maintaining the interior of the recording head 1201 at a negative pressure corresponding to the water 10 head H. In this manner the nozzle can be maintained in a state filled with ink and forming a meniscus at the aperture face.

The ink discharge from the nozzle is executed by driving the energy generating means thereby 15 pushing out the ink in the nozzle. After the ink discharge, the nozzle is filled with ink by the capillary force, from the side of the flow path 1201f. During the recording operation, the ink discharge from the nozzle and the ink filling into the nozzle 20 are repeated whereby the ink is sucked from time to time from the ink chamber 1205c through the supply tube 1206.

As the ink in the ink chamber 1205c is sucked into the recording head 1201 and the ink liquid level 25 in the ink chamber 1205c becomes lower than the lower end of the air introducing needle 1205b, air is introduced into the main tank 1204 through the air

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introducing needle 1205b. Along with this operation the ink in the main tank 1204 is introduced into the ink chamber 1205c whereby the lower end of the air introducing needle 1205b is immersed again in the ink in the ink chamber 1205c. Through the repetition of such operations, the ink in the main tank 1204 is supplied to the recording head 1201 along with the ink discharge therefrom.

In the sub tank 1201b of the recording head 1201, there are gradually accumulated gas entering the plastic material constituting the supply tube 1206 etc. and gas dissolved in the ink. In order to discharge useless gas accumulated in the sub tank 1201b, a gas discharge tube 1211 connected to a gas discharge pump 1211a is connected to the sub tank 1201b. However, in order to maintain the interior of the recording head 1201 at a suitable negative pressure, the discharge tube 1211 is provided with a valve 1211b, which is opened only in a gas discharging operation in such a manner that the pressure inside the recording head 1201 does not exceed the atmospheric pressure.

In order to eliminate viscosified ink clogging the ink discharge portion 1201g or a bubble generated from gas dissolved in the ink therein, the ink jet recording apparatus is usually provided with a recovery unit 1207, which is provided with a cap

1207a for capping the nozzle face of the recording head 1201 and a suction pump 1207c connected to the cap 1207a, and which eliminates the viscosified ink or accumulated bubble from the ink discharge portion 5 1201g by activating the suction pump 1207c thereby forcedly sucking the ink in the ink discharge portion 1201g.

In such suction recovery operation, a faster ink flow speed allows to effectively eliminate the viscosified ink and the bubble so that the cross 10 section of the flow path 1201f is made small in order to increase the ink flow speed therein. On the other hand, the cross section of the filter 1201c is made as large as possible as explained in the foregoing, 15 so that the flow path 1201f is made smaller in the cross section at the downstream side of the filter 1201c.

In the foregoing, there has been explained the conventional ink supply system in case of a tube 20 supply system, but, also in the integral head tank system, separated head tank system or pit-in system, the configuration at the downstream side of the filter of the recording head is basically same as in the above-described tube supply system, and the 25 difference lies only in the configuration of the ink supply path from the ink tank to the recording head.

However, the aforementioned conventional

configuration may be unable to completely eliminate
the bubbles, thereby eventually result in
deterioration of the recording quality such as by
discharge failure or ink dripping resulting from the
5 bubbles.

In the following there will be explained
drawbacks of the conventional configuration shown in
Fig. 25, when bubbles are accumulated in the ink flow
path 1201f at the downstream side of the filter 1201c.

10 A portion under the filter is reduced in the
cross section of the ink flow path and constitutes a
portion where the flow becomes stagnant even by the
recording operation of the recording head, so that
the bubbles tend to remain. Particularly in a
15 recording head designed for multiple nozzles and a
higher recording speed, the filter area has to be
increased so that the ink stagnant portion increases
in the ink flow, whereby the bubbles tend to remain
under the filter. Particularly in case the filter
20 and the ink flow path are positioned vertically with
respect to the direction of gravity, the bubbles
gather by the floating force under the filter.
However, a filter portion in contact with the bubbles
is incapable of filtering the ink, so that the
25 effective filter area is inevitably decreased.

Also the ink flow path, having a small cross
section, is clogged by a large bubble whereby the

substantial flow resistance increases to hinder the required ink supply to the nozzle, thus eventually resulting in ink dripping or the like.

Also the bubbles in the ink discharge portion
5 utilizing an electrothermal converting element as the energy generating means include those coming from the upstream side, namely those generated in ink passing through the filter, and those resulting from ink discharge, namely, after ink discharge by bubble
10 generation in the ink, those not dissolved again in the ink at the extinction of the bubble and gradually accumulated in the ink. Such bubble gradually grows and may enter the nozzle or may clog the connecting portion between the nozzle and the ink discharge
15 portion thereby resulting in discharge failure or ink dripping. Particularly in the vicinity of the ink discharge portion, fine bubbles tend to gather because the temperature in the vicinity of the heater rises to render re-dissolution of the bubbles into
20 the ink difficult, whereby the bubble tends to grow to a size causing detrimental effect on the recording.

Furthermore, in the conventional configuration, since the cross section of the ink flow path is reduced, the generated bubbles in the ink flow path
25 can be discharged by the recovery operation of the recording head, but the ink supply to the nozzle is hindered if the bubble grows so fast as to interrupt

the flow path. In order to avoid such situation, it is necessary to discharge the bubble by executing the recovery operation frequency, but there results a drawback that the ink is wasted at each recovery operation.

On the other hand, if the cross section of the ink flow path is so increased as "not to interrupt the ink flow path by the bubble" or "to eliminate a portion where the ink flow tends to become stagnant", the bubble becomes easily movable so that, even if the ink is strongly sucked in the suction recovery operation, there is only sucked the ink but the bubble itself merely moves upstream in the ink flow path and cannot be discharged by suction.

Also since the filter has a fine mesh structure, when the bubbles reach and are absorbed under the filter, there is formed a meniscus by the ink in the sub tank, in the space in the mesh of the filter. As a result, the bubbles under the filter cannot pass through the filter to the upstream side but are accumulated under the filter.

A filter portion under which the bubbles are accumulated cannot pass the ink, thereby reducing the effective area of the filter and increasing the ink flow resistance, whereby the ink supply amount from the sub tank to the ink flow path and the ink supply amount from the ink flow path to the ink discharge

portion become unbalanced to result in a discharge failure. Also, if the bubble accumulation in the ink supply portion and the deficient ink supply from the sub tank to the ink supply portion further proceed, 5 the ink in the ink discharge portion may result in a fatal drawback such as the ink supply to the nozzle being impossible.

Also in case the small bubbles accumulate under the filter grow to a large bubble, such large bubble 10 moves under the filter by the vibration of the recording head in the printing operation or the like, thereby securing, though unstably, an effective filter area for ink supply from the sub tank to the ink flow path, but, in case the small bubbles 15 accumulated under the filter do not assemble and remain as a gathered group of small bubbles, such small bubbles stick to the filter even under the vibration of the recording head in the printing operation or the like and do not easily move, whereby 20 the effective filter area for ink supply from the sub tank to the ink flow path becomes difficult to secure. Consequently there is encountered a situation where the ink supply to the nozzle cannot be realized.

Also, in order to avoid deterioration in the 25 recording quality such as discharge failure or ink dripping, resulting from such bubbles, it becomes necessary to frequently repeat the recovery operation

for removing the bubbles accumulating under the filter.

Such drawback is conspicuous in a recording head having a larger ink supply amount from the sub
5 tank to the ink flow path and tending to show a larger pressure loss in the filter, namely a recording head with multiple nozzles for recording with small dots.

10 SUMMARY OF THE INVENTION

The object of the present invention is to provide an ink jet recording head capable of preventing drawbacks resulting from the bubbles generated at the downstream side of the filter while
15 minimizing the waste of ink, an ink jet recording apparatus utilizing such ink jet recording head, a liquid supply system and a liquid filling method advantageously employable therein.

The above-mentioned object can be attained,
20 according to the present invention, by a liquid supply system which is provided with a liquid supply path to a liquid holding portion holding liquid at the downstream end in the liquid supply direction, and a filter in the liquid supply path and in which
25 the liquid can be supplied from the upstream side of the filter to the downstream side thereof in the vertical direction in the direction of gravity, the

system comprising:

a member for dividing a portion of the filter in contact with the downstream side into a gas holding area and a liquid holding area;

5 wherein the gas held in said gas holding area is in communication with gas present between the downstream side of the filter and the liquid holding portion in the aforementioned downstream end.

10 In the liquid supply system of the present invention, as the downstream side of the filter secures a gas holding area for holding gas, a bubble eventually generated at the downstream side of the filter, being smaller than the gas held in the gas holding area, is eventually united with such gas.

15 Thus it is rendered possible to avoid that the small bubbles are mixed in the liquid flow path or remain as a gathered group. Also the downstream side of the filter is divided into a gas holding area and a liquid holding area to stably secure an effective
20 filter area, whereby the liquid supply from the upstream side of the filter can be stably executed without deficiency even when the liquid of a large amount is consumed at the downstream end of the liquid supply path.

25 At the downstream side of the filter, there is preferably formed a liquid connecting structure for holding the liquid, present in the downstream side of

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the filter, by the surface tension in the gas holding area thereby being connected across the filter with the liquid at the upstream side thereof. In this manner, the liquid smoothly moves between the
5 upstream and downstream sides of the filter through the liquid connecting structure in case of liquid consumption at the downstream end of the liquid supply path or in case of a gas volume change in the gas holding area resulting for example from a change
10 in the environmental temperature.

The liquid connecting structure is preferably provided in the vertical direction and is provided with a groove-shaped structure of which the upper end is in contact with the downstream face of the filter.
15 In such case, the gap t between the groove-shaped structure and the filter is selected in a range $0 \leq t \leq 1.0$ mm whereby the liquid held by the groove-shaped structure is in satisfactory contact with the filter. Also in the downstream side of the filter, the liquid
20 supply path may be composed of a cover member constituting a lateral face thereof and a main body member constituting another face and jointed to the cover member, and the groove-shaped structure may be provided at least in the cover member. In such case,
25 the groove-shaped structure in the cover member may be formed as a projection with a slit, protruding from a joint plane of the cover member with the main

body member and adapted to hold liquid by the surface tension, whereby, even if the cover member and the main body member are jointed by an adhesive, the slit of the groove-shaped structure for holding liquid can
5 be prevented from entry of the adhesive.

Also the liquid supply path may be so constructed as to have a first liquid chamber at the upstream side of the filter and a second liquid chamber including the aforementioned gas holding area
10 at the downstream side of the filter. In such case, it is possible to form a valve mechanism at the upstream side of the first liquid chamber or to provide the first liquid chamber with an air communicating aperture which can be opened or closed,
15 whereby, in case the gas is accumulated in the second liquid chamber, suction is executed from the side of the second liquid chamber in a state where the valve mechanism or the air communicating aperture is closed, thereby reducing the pressure of the first and second
20 liquid chambers to a predetermined value, and then the valve mechanism or the air communicating aperture is opened to fill the first and second liquid chambers with liquid of respectively appropriate amounts from the upstream side, even when gas is
25 accumulated in the first and second liquid chambers to reduce the liquid amounts therein.

It is also possible to provide the liquid

supply path at the downstream side of the filter with two liquid chambers. By the gas inflation or the vapor pressure increase in the second liquid chamber, the liquid therein is pushed out to the downstream
5 end of the liquid supply path or returned to the first liquid chamber through the filter. However, an unexpected pushing out of the liquid in the second liquid chamber to the downstream end of the liquid supply path is undesirable, and the liquid in the
10 second liquid chamber cannot return to the first liquid chamber through the filter since, in the second liquid chamber, the filter is in contact with the gas holding area. Therefore, by forming a third liquid chamber having a liquid holding portion
15 adjacent to the gas in the gas holding area, the liquid held in the third liquid chamber can smoothly flow in the first liquid chamber through a contact portion with the filter even in case of gas inflation or vapor pressure increase in the second liquid
20 chamber, whereby the liquid in the second liquid chamber is not unexpectedly pushed out from the downstream end of the liquid supply path. The contact area of the liquid held in the third liquid chamber with the filter can be maintained constant
25 regardless of the liquid amount held in the third liquid chamber by providing the third liquid chamber with a desired number of liquid holding members. The

liquid holding on the liquid holding member can be achieved by utilizing the surface tension of the liquid.

According to the present invention there is
5 also provided an ink jet recording head provided with a first liquid chamber and a second liquid chamber separated by a filter and respectively containing liquid therein, and a liquid discharge portion connected directly with the second liquid chamber and
10 adapted to discharge the liquid supplied from the second liquid chamber, in which the liquid can be supplied from the first liquid chamber to the second liquid chamber through the filter, comprising:

a member for dividing a portion of the filter in
15 contact with the second liquid chamber into a gas holding area and a liquid holding area;

wherein the gas held in the gas holding area is in communication with the gas present in the second liquid chamber.

20 Also in the ink jet recording head of the present invention, since there are provided the first and second liquid chambers separated by the filter and the member for dividing the portion of the filter in contact with the second liquid chamber into the
25 gas holding area and the liquid holding area in a state capable of liquid supply from the first liquid chamber to the second liquid chamber and the gas held

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in the gas holding area is in communication with the gas present in the second liquid chamber, it is rendered possible to resolve the drawbacks resulting from the bubbles generated at the downstream side of the filter as in the aforementioned liquid supply system of the present invention, thereby enabling stable ink discharge from the discharge portion.

It is thus rendered possible to prevent deterioration in the recording quality such as discharge failure or so-called ink dripping, resulting from the bubbles, and also to reduce the number of recovery operations for eliminating the bubbles accumulated under the filter.

Also a configuration in which the liquid held in the liquid holding area is in communication with the second liquid chamber whereby the liquids in the first and second liquid chambers can reversibly move enables stable liquid discharge from the discharge portion even when the gas volume in the second liquid chamber repeats inflation and contraction.

According to the present invention, there is also provided an ink jet recording apparatus comprising:

support means for supporting the aforementioned ink jet recording head of the present invention;

suction means for forcedly sucking ink in the ink jet recording head from a liquid discharge portion

thereof; and

a valve mechanism for opening or closing of a first liquid chamber of the ink jet recording head to or from the exterior thereof.

5 In the ink jet recording apparatus of the present invention, being provided with the suction means and the valve mechanism, the suction means is at first activated in a state where the valve mechanism is closed, to reduce the pressure in the
10 ink jet recording head to a predetermined value, and then the valve mechanism is opened to fill the first and second liquid chambers with liquid of respectively appropriate amounts, even when gas is accumulated in the first and second liquid chambers
15 to reduce the liquid amounts therein.

According to the present invention there is also provided a liquid filling method for use in a liquid supply system in which the first and second liquid chambers respectively holding liquid are
20 separated by a filter while the liquid is held at the downstream side of the second liquid chamber in the liquid supply direction from the first liquid chamber to the second liquid chamber and gas is present in the gas holding area for separating the filter and
25 the liquid in the second liquid chamber in a state capable of liquid supply from the upstream side of the filter to the downstream side thereof, the method

comprising:

a step of closing the first liquid chamber from the exterior;

5 a step of executing suction from the downstream side of the second liquid chamber in a state where the first liquid chamber is closed, thereby reducing the pressure of the first and second liquid chambers; and

10 a step, after the pressure decrease of the first and second liquid chambers, of opening the first liquid chamber to the exterior.

It is thus rendered possible to fill the first and second liquid chambers with liquid of respectively appropriate amounts, even when gas is
15 accumulated in the first and second liquid chambers to reduce the liquid amounts therein.

BRIEF DESCRIPTION OF THE DRAWINGS

Fig. 1 is a perspective view showing the
20 schematic configuration of an ink jet recording apparatus constituting a first embodiment of the present invention;

Fig. 2 is a view showing an ink supply path for a color, in the ink jet recording apparatus shown in
25 Fig. 1;

Figs. 3A, 3B, 3C and 3D are views showing the behavior of gas and ink in the liquid path of an ink

supply unit, in case of gas introduction into a main tank in the ink supply path shown in Fig. 2;

Fig. 4 is a view showing a pressure formed by a water head on the nozzle, in the ink supply path
5 shown in Fig. 2;

Fig. 5 is a detailed cross-sectional view showing the internal configuration of the recording head shown in Fig. 2;

Fig. 6 is a perspective view, seen from above,
10 of the recording head shown in Fig. 2, in a state where an upper wall of a sub tank and a part of a filter are removed;

Fig. 7 is a cross-sectional view similar to Fig. 5, showing the ink flow from the sub tank to the
15 liquid chamber;

Fig. 8 is a cross-sectional view similar to Fig. 5, showing the flow of ink and gas in a closed state;

Fig. 9 is a view showing the ink supply path of an ink jet recording apparatus constituting a second
20 embodiment of the present invention;

Fig. 10 is a detailed cross-sectional view showing the internal configuration of the recording head shown in Fig. 9;

Fig. 11 is a perspective view, seen from above,
25 of the recording head shown in Fig. 9, in a state where an upper wall of a sub tank and a part of a filter are removed;

Fig. 12 is a view showing a variation of the recording head shown in Fig. 9;

Fig 13 is a lateral view showing the relationship between a groove structure and the filter in the upper end portion of a groove structure applicable in the present invention;

Figs. 14A, 14B and 14C are lateral views showing the joint structure of a filter applicable to the present invention;

Fig. 15 is a perspective view showing an example of the groove structure applicable to the present invention;

Figs. 16 to 22 are perspective views showing other examples of the groove structure applicable to the present invention;

Fig. 23 is a chart showing the relationship between an aperture width and an ink elevation height in various forms of the groove structure applicable to the present invention;

Fig. 24 is a perspective view of a cover member constituting the groove structure of the present invention; and

Fig. 25 is a view showing an ink supply system in an ink jet recording apparatus of conventional tube supply system.

DESCRIPTION OF THE PREFERRED EMBODIMENTS

Now the present invention will be clarified in detail by embodiments thereof, with reference to the accompanying drawings.

[First embodiment]

5 Fig. 1 is a perspective view showing schematic configuration of an ink jet recording apparatus constituting a first embodiment of the present invention.

203020" E233300T
10 The ink jet recording apparatus shown in Fig. 1 is a recording apparatus of serial type, capable of repeating the reciprocating motion (main scanning) of an ink jet head 201 and the conveying (sub scanning) of a recording sheet (recording medium) S such as an ordinary recording paper, a special paper, an OHP
15 film sheet etc. by a predetermined pitch and causing the ink jet head 201 to selectively discharge ink in synchronization with these motions for deposition onto the recording sheet S, thereby forming a character, a symbol or an image.

20 Referring to Fig. 1, the ink jet head 201 is detachably mounted on a carriage 201 which is slidably supported by two guide rails and is reciprocated along the guide rails by drive means such as an unrepresented motor. The recording sheet
25 S is conveyed by a conveying roller 203 in a direction crossing the moving direction of the carriage 202 (for example a perpendicular direction

A), so as to be opposed to an ink discharge face of the ink jet head 201 and to maintain a constant distance thereto.

The ink jet head 201 is provided with plural
5 nozzle arrays for discharging inks of respectively different colors. Corresponding to the colors of the inks discharged from the ink jet head 201, plural independent ink tanks 204 are detachably mounted on an ink supply unit 205. The ink supply unit 205 and
10 the ink jet head 201 are connected by plural ink supply tubes 206 respectively corresponding to the ink colors, and, by mounting the main tank 204 on the ink supply unit 205, the inks of respective colors contained in the main tank 204 can be independently
15 supplied to the nozzle arrays in the ink jet head 201.

In a non-recording area which is within the reciprocating range of the ink jet head 201 but outside the passing range of the recording sheet S, there is provided a recovery unit 207 so as to be
20 opposed to the ink discharge face of the ink jet head 201.

In the following there will be explained, with reference to Fig. 2, the detailed configuration of the ink supply system of the ink jet recording
25 apparatus. Fig. 2 is a view showing the ink supply path of the ink jet recording apparatus shown in Fig. 1, showing the path for a color for the purpose of

simplicity.

At first there will be explained the recording head 201.

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5 Ink is supplied to the recording head 201, from
a connector insertion port 201a to which hermetically
connected is a liquid connector provided on the end
of the ink supply tube 206. The connector insertion
port 201a communicates with a sub tank 201b formed in
the upper part of the recording head 201. In the
10 lower side of the sub tank 201b in the direction of
gravity, there is formed a liquid chamber 201f for
direct ink supply to a nozzle portion having plural
nozzles 201g arranged in a parallel manner. The sub
tank 201b and the liquid chamber 201f are separated
15 by a filter 201c, but, at the boundary of the sub
tank 201b and the liquid chamber 201f there is formed
a partition portion 201e having an aperture 201d, and
the filter 201c is provided on such partition portion
201e.

20 In the above-described configuration, the ink
supplied from the connector insertion port 201a to
the recording head 201 is supplied through the sub
tank 201b, filter 201c and liquid chamber 201f to the
nozzles 201g. The path between the connector
25 insertion port 201a to the nozzles 201g is maintained
in a hermetically tight condition to the atmosphere.

On the upper face of the sub tank 201b there is

formed an aperture which is covered by a dome-shaped elastic member 201h. The space surrounded by the elastic member 201h changes volume according to the pressure in the sub tank 201b and has a function of
5 adjusting the pressure in the sub tank 201b as will be explained later.

The nozzle 201g has a tubular structure of a cross-sectional width of about 20 μm and discharges ink by giving discharge energy to the ink therein,
10 and, after the ink discharge, the interior of the nozzle is filled with ink by the capillary force thereof. Normally the ink discharge is repeated with a cycle time of 20 kHz or higher, thereby achieving fine and high-speed image formation. For supplying
15 the ink in the nozzle 201g with the discharge energy, the recording head 201 is provided, in each nozzle 201g, with energy generation means. In the present embodiment, the energy generating means is composed of a heat generating resistor (electrothermal
20 converting element) for heating the ink in the nozzle 201g, and a command from a head control unit (not shown) for controlling the drive of the recording head 201 selectively drives the heat generating resistors thereby inducing film boiling of the ink in
25 the desired nozzle 201g, thereby discharging ink from the nozzle 201g by the pressure of a bubble formed by such film boiling.

The nozzle 201g is positioned with the ink discharging end (discharge port) downwards, but is not provided with a valve mechanism for opening or closing the discharge port, and the ink fills the nozzle 201g by forming a meniscus at the discharge port. For this purpose, the interior of the recording head 201, particularly the interior of the liquid chamber 201f, is maintained at a negative pressure relative to the atmospheric pressure.

However, if the negative pressure is excessively small, the meniscus at the ink discharge port may be broken in case a foreign substance or ink sticks to the end of the nozzle 201g, whereby ink may leak from the nozzle 201g. On the other hand, if the negative pressure is excessively large, the force retracting the ink into the nozzle 201g (or liquid chamber 201f) becomes stronger than the energy supplied to the ink at the discharge, thereby resulting in a discharge failure. Consequently the negative pressure in the liquid chamber 201f is maintained within a certain range somewhat lower than the atmospheric pressure. Such negative pressure, though dependent on the number and cross section of the nozzles 201g and the performance of the heat generating resistor, is preferably within a range from -20 mmAq (about -0.0020 atm = -0.2027 kPa) to -200 mmAq (about -0.0200 atm = -2.0265 kPa) (wherein the specific gravity of

ink being assumed equal to that of water) according to the experimental results of the present inventors.

In the present embodiment, the ink supply system 205 and the recording head 201 are connected by the ink supply tube 206 and the position of the recording head 201 relative to the ink supply unit 205 can be relatively freely selected, so that the recording head 201 is positioned higher than the ink supply unit 205 in order to maintain the interior of the recording head 201 at a negative pressure. Such height will be explained later in more details.

The filter 201c is composed of a metal mesh having fine holes not exceeding 10 μm and smaller than the cross sectional width of the nozzle 201g, in order to prevent leak of a substance that may clog the nozzle 201g, from the sub tank 201b to the liquid chamber 201f. The filter 201c has such a property that, when brought into contact with liquid on one surface thereof, each fine hole forms a meniscus of the ink by the surface tension thereof, whereby the gas flow through the filter becomes difficult. As the fine hole becomes smaller, the meniscus becomes stronger and the gas flow becomes more difficult.

In such filter 201c as employed in the present embodiment, the pressure required for passing gas is about 0.1 atm (10.1325 pKa: experimental value). Therefore, if gas is present in the liquid chamber

201f, present in the downstream side of the filter
201c in the ink moving direction in the recording
head, the gas cannot pass the filter 201c by the
floating force of the gas itself, and the gas in the
5 liquid chamber 201f remains therein. The present
embodiment utilizes this phenomenon in such a manner
that the liquid chamber 201f is not completely filled
with the ink but contains a gas layer between the ink
in the ink chamber 201f and the filter 201c, and the
10 liquid of a predetermined amount is contained in the
liquid chamber 201f in such a manner that the gas in
such gas holding area separates the ink in the liquid
chamber 201f and the filter 201c. The gas in such
gas holding area is so present in the liquid chamber
15 201f as to inhibit bubble movement from the nozzle
201g to the filter 201c.

The minimum necessary ink amount in the liquid
chamber 201f is an amount required for filling the
nozzle 201g with the ink. If gas enters the nozzle
20 201g from the liquid chamber 201f, the nozzle 201g
after ink discharge cannot achieve ink replenishment,
thus inducing discharge failure. Consequently the
interior of the nozzle 201g has to be always filled
with the ink.

25 The upper surface of the filter 201c is in
contact with the ink in the sub tank 201b, and the
ink can communicate through the filter 201c only in

an area where the ink on the upper surface of the filter 201c is in contact with that on the lower surface thereof, so that such communicable area constitutes the effective area of the filter 201c.

5 As already explained in the description of the prior art, the pressure loss in the filter 201c depends on the effective area thereof. In the present embodiment, the filter 201c of a large area is positioned substantially horizontally in the
10 operating state of the recording head 201 and the entire upper surface of the filter 201c is maintained in contact with the ink in order to increase the communicating area with the ink present at the lower surface of the filter, thereby maximizing the
15 effective area thereof and reducing the pressure loss.

The pressure adjusting chamber 201i reduces its volume as the internal negative pressure increases, and can be composed, as in the present embodiment, of an elastic member 201h which is preferably composed
20 of a rubber material or the like. The elastic member 201h can also be replaced by a combination of a plastic sheet and a spring. The volume of the pressure adjusting chamber 201i, being variable according to the ambient temperature in the operating
25 state of the recording head 201 and the volume of the sub tank 201b, is selected as about 0.5 ml in the present embodiment.

In the absence of the pressure adjusting chamber 201i, the pressure in the sub tank 201b is subjected directly to the resistance by the pressure loss when the ink goes through the main tank 204, ink supply unit 205 and ink supply tube 206. Therefore, in case of so-called high-duty ink discharge operation such as ink discharge from all the nozzles 201g, the ink amount supplied to the recording head 201 becomes deficient relative to the discharged ink amount, whereby the negative pressure increases rapidly. If the negative pressure of the nozzle 201g exceeds the aforementioned limit value of -200 mmAq (about -2.0265 kPa), the discharge becomes stable and unsuitable for image formation.

In the recording apparatus of serial scan type as in the present embodiment, even in the image formation with a high duty ratio, the ink discharge is interrupted at the inversion of the drive of the carriage 202 (Fig. 1). The pressure adjusting chamber 201i performs a function as in a capacitor of reducing the volume during the ink discharge to relax the increase in the negative pressure in the sub tank 201b and restoring the volume at the inversion of the movement of the carriage.

As an example, let us consider a case where the rate of change of the negative pressure with respect to the volume reduction in the pressure adjusting

chamber 201i is $K = -1.01325$ kPa/ml, while the sub
tank 201b has a volume $V_s = 2$ ml and the supplied ink
is deficient by $\Delta V = 0.05$ ml in comparison with the
discharged ink. In such case. if the pressure
5 adjusting chamber 201i is absent, based on the law of
"PV = constant", the negative pressure in the sub
tank 201i changes by $\Delta P = V_s / (V_s + \Delta V) - 1 = -2.47$
kPa, whereby the aforementioned limit value is
exceeded and the discharge becomes unstable. On the
10 other hand, in the presence of the pressure adjusting
chamber 201i, $\Delta P = K \times \Delta V = -0.51$ whereby the
increase of the negative pressure can be suppressed
and the discharge can be stabilized.

As explained in the foregoing, the pressure
15 adjusting chamber 201i allows to stabilize the ink
discharge and to suppress the influence of the
pressure loss in the ink supply path from the ink
tank 204 to the recording head 201. Therefore the
ink supply tube 206 moving along with the carriage
20 202 can also be of a smaller diameter, thus
contributing to reduce the moving load of the
carriage 202.

In the following there will be given an
explanation on the ink supply unit 205 and the main
25 tank 204.

The main tank 204 is constructed detachably
mountable on the supply unit 205 and is provided, on

the bottom portion thereof, with an ink supply aperture tightly closed with a rubber stopper 204b and an air introducing aperture tightly closed with a rubber stopper 204c. The main tank 204 is singly an
5 air-tight container, and the ink 209 is directly contained in the main tank 204.

On the other hand, the ink supply unit 205 is provided with an ink supply needle 205a for deriving ink 209 from the main tank 204, and an air
10 introducing needle 205b for introducing air into the main tank 204. The ink supply needle 205a and the air introducing needle 205b are both hollow needles and are positioned, with the front ends upwards, corresponding to the ink supply port and the air
15 introducing port of the main tank 204. When the main tank 204 is mounted on the ink supply unit 205, the ink supply needle 205a and the air introducing needle 205b respectively penetrate the rubber stoppers 204b, 204c, thus entering the interior of the main tank 204.

20 The ink supply needle 205a is connected, through a liquid path 205c, a shut-off valve 210 and a liquid path 205d, to the ink supply tube 206. The air introducing needle 205b is connected, through a liquid path 205e, a buffer chamber 205f and an air
25 communicating aperture 205g, to the external air. The liquid path 205c lowest in height within the ink supply path from the ink supply needle 205a to the

ink supply tube 206 and the liquid path 205e highest in height within the path from the air introducing needle 205b to the air communicating aperture 205g are positioned same in height. The ink supply needle 205a and the air introducing needle 205b in the present embodiment are composed of thick needles of an internal diameter of 1.6 mm and have needle holes of a diameter of 11.5 mm in order to suppress the flow resistance of the ink.

10 The shut-off valve 210 is provided with a rubber diaphragm 210a which is displaced to open or close the connection between the two liquid paths 205c, 205d. On the upper surface of the diaphragm 210a, there is mounted a tubular spring holder 210b
15 containing therein a compression spring 210c which serves to press the diaphragm 210a thereby closing the connection between the liquid paths 205c, 205d. The spring holder 210b is provided with a flange, engaging with a lever 210d to be operated by a link
20 207e of a recovery unit 207 to be explained later. By activating the lever 210d to lift the spring holder 210b against the spring force of the compression spring 210c, the connection between the liquid paths 205c, 205d is opened. The shut-off
25 valve 210 is opened during the ink discharge from the recording head 201 but is closed during a stand-by state or in a non-operated state, and is opened and

closed in synchronization with the recovery unit 207 during an ink filling operation to be explained later.

The above-described configuration of the ink supply unit 205 is provided for each main tank 204, namely for each ink color, except for the lever 210d. The lever 210d is provided common to all colors and simultaneously opens or closes the shut-off valves 210 for all the colors.

In the above-described configuration, when the ink is consumed in the recording head 201, the resulting negative pressure causes the ink to be from time to time supplied from the main tank 204 to the recording head 201 through the ink supply unit 205 and the ink supply tube 206. At this operation, air of an amount same as that of the supplied from the main tank 204 is introduced into the main tank 204 from the air communicating aperture 205g through the buffer chamber 205f and the air introducing needle 205b.

The buffer chamber 205f provides a space for temporarily holding the ink flowing out of the main tank 204 by the inflation of gas in the main tank 204, and the lower end of the air introducing needle 205b is positioned at the bottom of the buffer chamber 205f. In case the gas in the main tank 204 expands by an increase in the ambient temperature or a decrease in the external pressure during a stand-by

state or a pause of the ink jet recording apparatus,
since the shut-off valve 210 is closed, the ink in
the main tank 204 flows out to the buffer chamber
205f through the air introducing needle 205b and the
5 liquid path 205e. On the other hand, the gas in the
main tank 204 contracts for example by a decrease in
the ambient temperature, the ink flowing out in the
buffer chamber 205f returns to the main tank 204.
Also in case the recording head discharges ink while
10 the ink is present in the buffer chamber 205f, at
first the ink in the buffer chamber 205f returns to
the main tank 204 and the gas is introduced into the
main tank 204 after the ink in the buffer chamber
205f is depleted.

15 The volume V_b of the buffer chamber 205f is so
selected as to satisfy the environmental use
condition of the product. For example, for a product
to be used within a temperature range of 5°C (278K)
to 35°C (308K), and for a main tank 204 having a
20 volume of 100 ml, the volume V_b is selected as $100 \times$
 $(308 - 278)/308 = 9.7$ ml or larger.

Now there will be explained, with reference to
Figs. 3A to 3D, the basic water head of the main tank
204 and the behavior of gas and ink in the liquid
25 path of the ink supply unit 205 at the gas
introduction into the main tank 204.

Fig. 3A shows a normal state capable of ink

supply from the main tank 204 to the recording head
201 (cf. Fig. 2). In this state, the interior of the
main tank 204 is maintained air-tight except for the
buffer chamber 205f and is maintained at a negative
5 pressure relative to the atmospheric pressure, and
the front end 209a of the ink remains in the liquid
path 205e. The front end of the ink is in contact
with air and is therefore at the atmospheric pressure
(= 0 mmAq). The liquid path 205c in which the front
10 end 209e of the ink is positioned and the liquid path
205e communicating with the ink supply tube 205 (cf.
Fig. 2) are of a same height and mutually communicate
only through the ink, so that the pressure of the
liquid path 205e is also the atmospheric pressure.
15 This pressure is determined only by the height
relationship of the front end 209a of the ink and the
liquid path 205c and is influenced by the amount of
ink 209 in the main tank 204.

As the ink in the main tank 204 is consumed,
20 the front end 209a of the ink gradually move toward
the air introducing needle 205b as shown in Fig. 3B,
and, upon reaching a position directly below the air
introducing needle 205b, the air floats as a bubble
in the air introducing needle 205b as shown in Fig.
25 3C and introduced into the main tank 204. In return,
the ink in the main tank 204 enters the interior of
the air introducing needle 205b, whereby the front

end 209a of the ink returns to the original state shown in Fig. 3A.

Fig. 3D shows a state where ink is accumulated in the buffer chamber 205f. In this state, the front
5 end 209a of the ink is at a position in the middle of the height of the buffer chamber 205f and higher than the liquid path 205c by h_1 (mm) so that the pressure in the liquid path 205c is $-h_1$ (mmAq).

Thus, in the present embodiment, the negative
10 pressure P_n applied to the lower end of the nozzle 201g (cf. Fig. 2) by the water head is $P_n \approx -9.8 \times (h_2 - h_3 - h_4)$ Pa in the normal state or $-9.8 \times (h_2 - h_1 - h_3 - h_4)$ Pa in a state where the ink is accumulated in the buffer chamber 205f, wherein h_2 (mm) is the
15 height from the liquid path 205c to the upper face 209b in the sub tank 201b as shown in Fig. 4, h_3 (mm) is the height from the filter 201c to the upper face 209b in the sub tank 201b and h_4 (mm) is the height from the lower end of the nozzle 201g to the upper
20 face 209c in the liquid chamber 201f. The value P_n is so selected as to be contained within the aforementioned negative pressure range of $(-0.2027$ to -2.0265 kPa).

Again referring to Fig. 2, the ink supply
25 needle 205a and the air introducing needle 205b are connected to a circuit 205h for measuring the electrical resistance of the ink, thereby detecting

the presence or absence of ink in the main tank 204. The circuit 205h detects an electrically closed state in the presence of ink in the main tank 204 since a current flows in the circuit 205h through the ink in the main tank 204, but an electrically open state in the absence of ink or in case the main tank 204 is not mounted. Since the detected current is very weak, the insulation between the ink supply needle 205a and the air introducing needle 205b is important. In the present embodiment, the path from the ink supply needle 205a to the recording head 201 is made completely independent from the path from the air introducing needle 205b to the air communicating aperture 205g, whereby it is rendered possible to measure the electrical resistance of the ink only in the main tank 204.

In the following there will be given an explanation on the recovery unit 207.

The recovery unit 207 serves to suck ink and gas from the nozzle 201g and to operate the shut-off valve 210, and is provided with a suction cap 207a for capping the ink discharge face (containing aperture of the nozzle 201g) of the recording head 201, and a link 207e for operating the lever 210d of the shut-off valve 210.

The suction cap 207a is composed of an elastic member such as of rubber at least in a portion coming

into contact with the ink discharge face, and is rendered movable between a position for tightly closing the ink discharge face and a position retracted from the recording head 201. The suction
5 cap 207a is connected to a tube having a suction pump 207c of tube pump type in an intermediate position thereof, and is capable of continuous suction by activating the suction pump 207c by a pump motor 207d. It is also possible to vary the suction amount by
10 changing the revolution of the pump motor 207d. The present embodiment employs a suction pump 207c capable of reducing pressure to -0.8 atm (81.060 kPa).

A cam 207b for activating the suction cap 207a is rotated by a cam control motor 207g, in
15 synchronization with a cam 207f for operating the link 207e. The timing of the cam 207b coming into contact with the suction cap 207a in the positions a to c corresponds to the timing of the cam 207f coming into contact with the link 207e in the positions a to
20 c. In the position a, the cam 207b separates the suction cap 207a from the ink discharge face of the recording head 201, and the cam 207f presses the link 207e to elevate the lever 210d, thereby opening the valve 210. In the position b, the cam 207g brings
25 the suction cap 207a in contact with the ink discharge face, and the cam 207f pulls back the link 207e to close the valve. In the position c, the cam

207b brings the suction cap 207a in contact with the ink discharge face, and the cam 207f presses the link 207e to open the valve.

In the recording operation, the cams 207b, 207f
5 are maintained in a state of the position a to enable ink discharge from the nozzle 201g and ink supply from the main tank 204 to the recording head 201. In a non-operating state including a stand-by state and a pause, the cams 207b, 207f are maintained in a
10 state of the position b to prevent drying of the nozzle 201g and ink flow-out from the recording head 201 (particularly in case the apparatus itself is moved, the apparatus may be inclined to induce ink flow-out). The position c of the cams 207b, 207f is
15 employed in an ink filling operation to the recording head 201 to be explained later.

In the foregoing there has been explained the ink supply path from the main tank 204 to the recording head 201, but the configuration shown in
20 Fig. 2 eventually results in gas accumulation in the recording head 201 over a prolonged period.

In the sub tank 201b, there are accumulated gas permeating through the ink supply tube 206 and the elastic members 201h, and gas dissolved in the ink.
25 The gas permeating through the ink supply tube 206 and the elastic member 201h can be prevented by employing a material of high gas barrier property,

but such material is expensive. In the mass produced consumer equipment, it is not easy to use expensive material in consideration of the cost. In the present embodiment, the ink supply tube 206 is
5 composed of a polyethylene tube of low cost and high flexibility, and the elastic member 201h is composed of butyl rubber.

On the other hand, in the liquid chamber 201f, there is gradually accumulated gas, because of a
10 phenomenon that the bubble generated in the ink discharge from the nozzle 201g, namely the bubble generated in the ink in the nozzle 201g in the recording operation but thereafter not re-dissolved in the ink at the contraction of the bubble and
15 returning to the liquid chamber 201f, or a phenomenon that the fine bubbles present in the ink gather to form a larger bubble by an increase of the ink temperature in the nozzle 201g.

According to the experiment of the present
20 inventors, in the configuration of the present embodiment, the gas accumulates by about 1 ml/month in the sub tank 201b and about 0.5 ml/month in the liquid chamber 201f.

The gas accumulation in the sub tank 201b and
25 the liquid chamber 201f reduces the ink amount therein. In the sub tank 201b, an ink deficiency causes exposure of the filter 201c to the gas to

reduce the effective area thereof, thereby increasing the pressure loss thereof and eventually disabling ink supply to the liquid chamber 201f. Also an ink deficiency in the liquid chamber 201f causes exposure
5 of the upper end of the nozzle 201g to the gas, thereby rendering ink supply thereto impossible. In this manner, a fatal situation arises unless each of the sub tank 201b and the liquid chamber 201f contains ink at least equal to a predetermined amount.

10 Therefore, by filling each of the sub tank 201b and the liquid chamber 201f with an appropriate amount of ink at a predetermined interval, the ink discharging performance can be stably maintained over a long period, even without employing the material of
15 high gas barrier property. For example, in the present embodiment, the sub tank 201b and the liquid chamber 201f may be filled with ink every month by an amount equal to the accumulating gas amount per month plus fluctuation in the filling.

20 The ink filling into the sub tank 201b and the liquid chamber 201f is executed utilizing the suction operation by the recovery unit 207. More specifically, the suction pump 207c is activated in a state where the ink discharge face of the recording
25 head 201 is tightly closed by the suction cap 207a, thereby sucking the ink in the recording head 201 from the nozzle 201g. However, in simple ink suction

from the nozzle 201g, ink of an amount approximately equal to the ink sucked from the nozzle 201g flows from the sub tank 201b into the liquid chamber 201f and ink of an amount approximately equal to that
5 flowing out of the sub tank 201b flows from the main tank 204 into the sub tank 201b, so that the situation does not change much from the state prior to suction.

Therefore, in the present embodiment, in order
10 to fill the sub tank 201b and the liquid chamber 201f separated by the filter 201c respectively with appropriate amounts of ink, the sub tank 201b and the liquid chamber 201f are reduced to a predetermined pressure utilizing the shut-off valve 210, thereby
15 setting the volumes of the sub tank 201b and the liquid chamber 201f.

In the following there will be explained the ink filling operation of the sub tank 201b and the liquid chamber 201f, and the volume setting thereof.

20 In the ink filling operation, at first the carriage 202 (cf. Fig. 1) is moved to a position where the recording head 120 is opposed to the suction cap 207a, and the cam control motor 207g of the recovery unit 207 is activated to rotate the cams
25 207b, 207f to a state where the position b for respective contacts with the suction cap 207a and the link 207e. Thus the ink discharge face of the

recording head 201 is closed by the suction cap 207a, and the shut-off valve 210 closes the ink path from the main tank 204 to the recording head 201.

The pump motor 207d is activated in this state
5 to execute suction by the suction pump 207c from the suction cap 207a. This suction operation sucks ink and gas, remaining in the recording head 201, through the nozzle 201g, thereby reducing the pressure in the recording head 201. The suction pump 207c is stopped
10 when the suction reaches a predetermined amount, and the cam control motor 207g is activated to rotate the cams 207b, 207f to a state where the position c in contact with the suction cap 207a and the link 207e. Thus the ink discharge face remains in the closed
15 state by the suction cap 207a but the shut-off valve 210 is opened. The suction amount of the suction pump 207c is so selected as to bring the interior of the recording head 201 to a predetermined pressure required for filling the sub tank 201b and the liquid
20 chamber 201f with ink of appropriate amounts, and can be determined by calculation or by experiment.

As the internal pressure of the recording head 201 is reduced, ink flows into the recording head 201 through the ink supply tube 206, thereby filling each
25 of the sub tank 201b and the liquid chamber 201f with ink. The amount of ink filling corresponds to a volume required for returning the sub tank 201b and

the liquid chamber 201f to the atmospheric pressure,
and is determined by the volume and pressure thereof.

The ink filling into the sub tank 201b and the
liquid chamber 201f is completed in about 1 second
5 after opening the shut-off valve 210. Upon
completion of the ink filling, the cam control motor
207g is driven to rotate the cams 207g, 207f to a
state where the position a is in contact with the
suction cap 207a and the link 207e. In this manner
10 the suction cap 207a is separated from the recording
head 201, and the suction pump 207c is activated
again to suck the ink remaining in the suction cap
207a. As the shut-off valve 210 is open in this
state, the recording head 201 can discharge ink to
15 form a character or an image on the recording sheet S
(cf. Fig. 1). In a stand-by state or in a pause, the
cam control motor 207g is activated again to rotate
the cams 207b, 207f to a state where the position b
is in contact with the suction cap 207a and the link
20 207e, thereby closing the ink discharge face of the
recording head 201 with the suction cap 207a and
closing the shut-off valve 210.

Unless the ink in the sub tank 201b and the
liquid chamber 201f becomes deficient over a long
25 period, it is not necessary to frequently execute the
suction operation by the recovery unit 207, so that
the chances of wasting ink can be reduced. Also the

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ink filling, if required in both of the sub tank 201b and the liquid chamber 201f, can be achieved in a single filling operation, thereby allowing to economize the ink.

5 Now, let us consider the relationship among the volume V_1 of the sub tank 201b, the ink amount S_1 to be filled therein and the pressure P_1 (relative to the atmospheric pressure) therein. Based on the law "PV = constant", the sub tank 201b can be filled with
10 the ink of an appropriate amount in the filling operation, by setting a relation $V_1 = S_1/|P_1|$. Similarly, for the volume V_2 of the liquid chamber 201f, the ink amount S_2 to be filled therein and the pressure P_2 (relative to the atmospheric pressure)
15 therein, the liquid chamber 201f can be filled with the ink of an appropriate amount in the filling operation, by setting a relation $V_2 = S_2/|P_2|$.

Also the filter 201c separating the sub tank 201b and the liquid chamber 201f has a fine mesh
20 structure and the gas flow therein is difficult in a state having a meniscus therein, as explained in the foregoing. For a pressure P_m required for gas permeation through the filter 201c having such meniscus, in case of suction from the nozzle 201g by
25 the recovery unit 207, the pressure P_2 in the liquid chamber 201f becomes lower by P_m than the pressure P_1 in the sub tank 201b since the gas has to come

from the sub tank 201f through the filter 201c. Thus,
by employing this relationship in determining the
volumes of the sub tank 201b and the liquid chamber
201f, the condition of the filling operation can be
5 easily determined.

In the following there will be explained
specific examples of the aforementioned filling
operation and the volume setting.

It is assumed that the ink filling is executed
10 every month, and the gas accumulating amount per
month is 1 ml in the sub tank 201b and 0.5 ml in the
liquid chamber 201f. It is also assumed that the ink
amount required in the sub tank 201b not to expose
the filter 201c to gas is 0.5 ml while the ink amount
15 required in the liquid chamber 201f not to expose the
nozzle 201g to gas is 0.5ml, and the fluctuation in
the ink filling amount is 0.2 ml both in the sub tank
201b and the liquid chamber 201f. Thus the ink
amount to be filled in a single filling operation is
20 the sum of these amounts, and is 1.7 ml in the sub
tank 201b and 1.2 ml in the liquid chamber 201f.

The reduced pressure in the recording head 201
is selected within the ability of the recovery unit
207. In the present embodiment, since the power
25 limit of the suction pump 207c is -0.8 atm (81.060
kPa), the suction amount of the suction pump 207c is
experimentally so determined that the pressure in the

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suction cap 207a can reach -0.5 atm (-50.6625 kPa) with a margin, and is controlled by the revolution of the pump motor 207d.

As the pressure required for gas permeation
5 against the meniscus in the nozzle 201g is
experimentally -0.05 atm (-5.06625 kPa), there is
generated a difference between the pressures of the
suction cap 207a and the liquid chamber 201f by the
resistance of the nozzle 201g, whereby the pressure
10 in the liquid chamber 201f becomes higher than that
in the suction cap 207a by 0.05 atm (5.06615 kPa).
Similarly, as the pressure required for gas
permeation against the meniscus in the filter 201 c
is experimentally -0.1 atm (-10.1325 kPa), there is
15 generated a difference between the pressures of the
liquid chamber 201f and the sub tank 201b by the
resistance of the filter 201c, whereby the pressure
in the sub tank 201b becomes higher than that in the
liquid chamber 201f by 0.1 atm (10.1325 kPa).
20 Therefore, by setting the pressure in the suction
capo 207a at -0.5 atm (-50.6625 kPa), the pressure in
the liquid chamber 201f becomes -0.45 atm (-45.5963
 kPa) while that in the sub tank 201b becomes -0.35
 atm (-35.4638 kPa).

25 In order to fill the sub tank 201b with ink of
1.7 ml, the volume V1 thereof is so selected that the
internal pressure becomes -0.35 atm (-35.4638 kPa)

when ink of 1.7 ml is sucked from the sub tank 201b having an internal pressure of about 1 atm (101.325 kPa). Thus, $V_1 = 1.7/0.35 = 4.85$ ml. Similarly the volume V_2 of the liquid chamber 201f can be

5 determined as $V_2 = 1.2/0.45 = 2.67$ ml.

After the internal pressure of the recording head 201 is reduced under the foregoing conditions, the shut-off valve 210 is opened whereby the ink flows into the recording head 201 in a reduced
10 pressure state. More specifically, at first the ink flows into the sub tank 201b whereby the gas inflated to the volume V_1 under reduced pressure is restored almost to the atmospheric pressure. The gas volume V_{1a} in the sub tank 201b in such state is given by
15 $V_{1a} = V_1 \times (1 - 0.35) = 3.15$ ml, and the filling is terminated when ink in an amount of $V_1 - V_{1a} = 1.7$ ml is filled into the sub tank 201b. Similarly, in the liquid chamber 201f, the ink flows from the sub tank 201b whereby the gas inflated to the volume V_2 under
20 reduced pressure is restored almost to the atmospheric pressure. The gas volume V_{2a} in the liquid chamber 201f in such state is given by $V_{2a} = V_2 \times (1 - 0.45) = 1.47$ ml, and the filling is
25 terminated when ink in an amount of $V_2 - V_{2a} = 1.2$ ml is filled into the liquid chamber 201f.

Thus, by setting the volumes and reduced pressures of the sub tank 201b and the liquid chamber

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201f in the above-described manner, it is rendered possible to fill the sub tank 201b and the liquid chamber 201f, separated by the filter 201c, with the ink of appropriate amounts in a single filling operation, so that the recording head can be properly operated over a long period even in a situation where gas is accumulated therein.

Also, as explained in the foregoing, gas of the gas holding area is present between the filter 201c and the upper surface of the ink in the liquid chamber 201f, but the gas volume in such gas holding area can be arbitrarily set by the suction pressure in the suction operation of the recovery unit 207. Thus, the gas in the gas holding area is manageable in the volume thereof.

It is thus rendered possible to significantly improve the reliability against the discharge failure resulting from the bubble generated between the filter and the nozzle. More specifically, against the conventional drawback that the effective area of the filter changes (decreases) by the presence of the unmanageable bubbles under the filter, the present embodiment provides a configuration where the lower surface of the filter 201c is in contact, from the beginning, with the gas of the gas holding area in the managed portion (aperture 201d in Fig. 2) so that the effective area of the filter 201c scarcely

changes.

Therefore, the necessary effective area of the filter 201c can be controlled in consideration of the above-mentioned fact in the design stage, whereby the reliability can be improved.

Also against the drawback that the bubble clogs the flow path between the filter and the nozzle, the cross sectional area of the liquid chamber 201f is selected sufficiently large with respect to the diameter of the bubble that can exist in the liquid chamber 201f, so that the ink flow cannot be hindered by the bubble in the liquid chamber 201f.

Furthermore, against the drawback that the bubble in the liquid chamber enters the nozzle or clogs the connection between the liquid chamber and the nozzle, the cross sectional area of the liquid chamber 201f is selected sufficiently large as explained in the foregoing, so that the bubble generated in the liquid chamber 201f rises by the floating force thereof in the ink in the liquid chamber 201f and is united with the gas in the gas holding area, thereby being prevented from entering the nozzle 201g. Besides, even if the bubble generated in the liquid chamber 201f is united with the gas of the gas holding area, the effective area of the filter 201c does not change since the gas in the gas holding area is manageable as explained

before.

Thus, by constructing the liquid chamber 201f separated from the sub tank 201b by the filter 201c in the above-described manner, it is rendered
5 possible to significantly improve the reliability against the discharge failure resulting from the bubble generation in the liquid chamber 201f or from the movement of the generated bubble.

In the following there will be explained other
10 features of the present invention.

In the configuration of the present embodiment, when the shut-off valve 210 is closed, the interior of the recording head 201 is a closed system in which the ink is held by the meniscus pressure at the
15 surface of the nozzle 201g. In the following there is considered a situation where the shut-off valve 210 is closed at a low temperature and then the ambient temperature increases. In such case, in the sub tank 201b which is opposed to the nozzle 201g
20 across the filter 201c, there are generated gas inflation and a rise in the vapor pressure, because of the rise in temperature and the decrease in the external pressure. Such gas inflation and the rise in vapor pressure can be absorbed by the pressure
25 adjusting chamber 201i.

However, the liquid chamber 201f, positioned at the side of the nozzle 201g with respect to the

filter 201c, is not connected with a space such as the pressure adjusting chamber 201i, for absorbing the gas inflation or the rise in vapor pressure but has a constant volume. The liquid chamber 201f, being directly connected with the nozzle 201g, cannot contain even very small particle. Though it is theoretically possible to provide the liquid chamber 201f with a space similar to the pressure adjusting chamber 201i, the presence of a member susceptible to generate impurity or particle upon deformation, such as rubber, in the liquid chamber 201f is impractical in consideration of the manufacturing cost.

Therefore, the gas inflated in the liquid chamber 201f pushes out the ink therein to the exterior thereof. In such situation, if the ink in the liquid chamber 201f is even partially in contact with the filter 201c, for example along the wall of the liquid chamber 201f by the surface tension, the ink can pass through the filter 201c and can escape into the sub tank 201b.

However, in case the entire surface of the filter 201c at the side of the liquid chamber 201f is exposed to the gas and is not in contact with the ink, the filter 201c holds the meniscus by the contact with the ink at the side of the sub tank 201b, so that the ink cannot escape to the sub tank 201b unless such meniscus is broken.

On the other hand, the meniscus is also held in the nozzle 201g, and, if the holding force for such meniscus at the nozzle 201g is smaller than that for the meniscus at the filter 201c, the ink leaks from the nozzle 201g. Moreover, the meniscus in the nozzle 201g, if once broken, cannot be easily restored, so that the ink in the liquid chamber 201f blows out by an amount corresponding to the gas inflation or increase in vapor pressure.

In the present embodiment, in order to prevent such drawback, the partition portion 201e provided at the boundary of the sub tank 201b and the liquid chamber 201f and supporting the filter 201c is so structured that the ink is securely in contact with the face of the filter 201c at the side of the liquid chamber 201f. In this manner the "force breaking the meniscus formed on the nozzle 201g" is made equal to or larger than the "ink moving force to the filter 201c" thereby preventing the ink leakage from the nozzle 201g. Such structure will be explained in the following with reference to Figs. 5 and 6.

Fig. 5 is a cross-sectional view showing the detailed internal structure of the recording head shown in Fig. 2, and Fig. 6 is a perspective view, seen from above, of the recording head shown in Fig. 2 in a state where the upper wall of the sub tank and a part of the filter are eliminated. In Fig. 5, the

detailed cross-sectional structure of the nozzle 201g is omitted.

As shown in Figs. 5 and 6, in the peripheral portion of the partition portion 201e, there is
5 formed a lateral wall 221a extending toward the sub tank 201b, and the filter 201c is in fact placed on the lateral wall 221a. In this manner, the ink can also be held in an area surrounded by the lateral wall 221a. Stated differently, the partition portion
10 201e constitutes an auxiliary liquid chamber between the sub tank 201b and the liquid chamber 201f. The height of the lateral wall 221a is so selected that the ink held in the partition portion 201e can always contact the lower surface of the filter 201c by the
15 surface tension (in the drawing, for the purpose of clarity, the ink held in the area surrounded by the lateral wall 221a contacts, in a major portion, the lower surface of the filter 201c by surface tension.

Inside the area surrounded by the lateral wall
20 221a, there are provided plural ribs 221c, 221d, of which height is same as that of the lateral wall 221a and of which upper ends also contact the lower surface of the filter 201c. Thus, the ink rising along the ribs 221c, 221d by the capillary phenomenon
25 also comes into contact with the lower surface of the filter 201c, thereby increasing the amount of the ink in contact with the lower surface thereof.

In the periphery of the aperture 201d, the lateral wall 221a is made lower in at least a part thereof. Such lower portion of the lateral wall 221a is not in contact with the filter 201c, and the interior of the partition portion 201e and the liquid chamber 201f mutually communicate through such portion. In this manner it is rendered possible to secure the gas holding area.

In the above-described configuration, as the ink in the liquid chamber 201f is consumed by the ink discharge from the nozzle 201g, the negative pressure in the liquid chamber 201f gradually increases. As the liquid chamber 201f communicates with the interior of the partition portion 201c, the negative pressure therein also increases like the negative pressure in the liquid chamber 201f.

The negative pressure increase in the liquid chamber 201f and the interior of the partition portion 201e causes the ink to flow into the liquid chamber 201f from the sub tank 201b through the filter 201c. In this operation, since the ink held by 221a, 221c, 221d etc. in the partition portion 201e is in contact with the lower surface of the filter 201c by the surface tension, the ink flow is facilitated in such portion. Consequently, as indicated by an arrow in Fig. 7, the ink in the sub tank 201b flows from a portion, in contact with the

ink, of the lower surface of the filter 201c into the partition portion 201e through the lateral wall 221a and the ribs 221c, 221d, and the ink thus flowing in overflows from the lateral wall 221a around the
5 aperture 201d to enter the liquid chamber 201f.

Now there will be explained, with reference to Fig. 8, the ink flow in case of gas inflation or an increase in the vapor pressure in the recording head 201, induced for example by an increase in the
10 ambient temperature or a decrease in the external pressure while the shut-off valve 210 (cf. Fig. 2) is closed.

In case of gas inflation or an increase in the vapor pressure in the liquid chamber 201f, the gas of
15 a volume corresponding to such inflation or pressure increase has to either escape to the sub tank 201b through the filter 201c or push out the ink (including the ink in the partition portion 201e) in the liquid chamber 201f to the exterior, but, in
20 practice, the latter situation takes place because it is difficult for the gas in the liquid chamber 102f to pass through the filter 201c in contact with the ink in the sub tank 201b as already explained before. However, in the partition portion 201e, the ink held
25 by the components 221a, 221c, 221d etc. is in contact with the filter 201c by the surface tension and the ink can easily pass through the filter 201c in such

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contact portion thereof. Thus, in case of gas
inflation or an increase in the vapor pressure in the
liquid chamber 201f, the ink in the partition portion
201e flows into the sub tank 201b through the lateral
5 wall 221a or the ribs 221c, 221d and the filter 201c.

On the other hand, the sub tank 201b, being
provided with the pressure adjusting chamber 201i as
explained in the foregoing, can absorb the volume
increase resulting from the ink flow through the
10 filter 201c as a result of gas inflation or an
increase in the vapor pressure in the liquid chamber
201f.

In such situation, in order that the ink in the
partition portion 201e is not depleted, the ink
15 holding volume V_f in the partition portion 201e and
the maximum gas volume increase ΔV_{max} in the liquid
chamber 201f have to satisfy a relation $V_f > \Delta V_{max}$.
The value ΔV_{max} can be given by (the gas volume in
liquid chamber 201f) \times (estimated maximum temperature
20 change ratio) in case the gas inflation or the
increase in the vapor pressure in the recording head
201 is induced by a temperature increase.

Since the above-described configuration of the
partition portion 201e allows to maintain the surface
25 of the filter 201c at the side of the liquid chamber
201f always in contact with the ink, even in case of
gas inflation or an increase in the vapor pressure in

the liquid chamber 201f, the ink of an amount corresponding to the gas volume increase can be moved smoothly to the sub tank 201b through the filter 201c, thereby preventing the ink blow-out phenomenon from the nozzle 201g. Besides, as the contact of the ink with the filter 201c in the partition portion 201e is achieved by the capillary phenomenon by the lateral wall 221a and the ribs 221c, 221d, there cannot be generated a bubble in such contact portion.

10 Furthermore, the effective area of the filter 201c remains substantially constant, because the contact between the ink and the lower surface of the filter 201c is made in a predetermined area.

Also in the present embodiment, the structure for contacting ink with the surface of the filter 201c at the side of the liquid chamber 201f is constructed utilizing the partition portion 201e in which the filter 201c is provided, and can therefore be realized easily and inexpensively without requiring special members or special manufacturing steps. The ribs 221c, 221d are not particularly limited in number or position, but, it is preferred to increase the number of the ribs and to reduce the gaps thereof in order to hold a larger amount of ink in the partition portion 201e and to contact a larger amount of ink with the filter 201c.

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The position of the aperture 201d can be

arbitrarily selected in the partition portion 201e,
but, in order that the entire periphery of the
aperture 201d can be utilized as a lateral wall for
generating capillary phenomenon, it is preferable to
5 form the aperture 201d in a position separated from
the internal wall of the sub tank 201b or the liquid
chamber 201f thereby forming the partition portion
201e as a kind of corridor structure having the
aperture 201d at the center. Also in case a small
10 ink holding amount is enough in the partition portion
201e, it is also possible to form the partition
portion 201e as a flat plate shape for supporting the
filter 201c in a planar manner and to generate the
capillary phenomenon directly in such supporting area.

15 [Second embodiment]

Fig. 9 is a view showing the ink supply path in
an ink jet recording apparatus constituting a second
embodiment of the present invention, while Fig. 10 is
a cross-sectional view showing the detailed internal
20 structure of the recording head shown in Fig. 9, and
Fig. 11 is a perspective view, seen from above, of
the recording head shown in Fig. 9 in a state where
the upper wall of the sub tank and a part of the
filter are eliminated. In Fig. 10, the detailed
25 cross-sectional structure of the nozzle 301g is
omitted.

The ink jet recording apparatus of the present

embodiment is also an ink jet recording apparatus of serial scan type as in the first embodiment, and has an entire configuration similar to that shown in Fig. 1. Also the present embodiment is similar to the first embodiment in forming a color image by discharging inks of plural colors, but Fig. 9 shows, as in Fig. 2, the ink supply path for a color only.

In the present embodiment, the configuration of the recording head 301 is different from that in the first embodiment. However, it is similar to the first embodiment in other aspects, such as that the ink supply to the recording head 301 is executed from a main tank 304 through an ink supply unit 305 and an ink supply tube 306, and that a recovery unit 307 having a suction cap 307a and a suction pump 307b is provided for forcibly sucking ink from a nozzle 301g of the recording head 301 at the ink filling into the recording head 301 or at the elimination of viscosified ink etc. from the recording head 301. Also the configuration of the main tank 304, ink supply unit 305, ink supply tube 306 and recovery unit 307 is similar to that in the first embodiment. Therefore, in the following, the description will omit these same or similar aspects and will be concentrated on the recording head 301.

The recording head 301 is provided with a sub tank 301b having a connector inserting port 301a in

which the liquid connector of the ink supply tube 306 is connected and a pressure adjusting chamber 301i, a liquid chamber 301f provided gravitationally below the sub tank 301b and serving to directly supplying the nozzle 301g with ink, and a filter 301c provided between the sub tank 301b and the liquid chamber 301f. In the liquid chamber 301f, a gas holding area is formed between the ink in the liquid chamber 301f and the filter 301c, by the liquid chamber 301f, filter 301c and a liquid chamber groove structure 301j, for securing gas so as to intercept the bubble movement from the nozzle 301g to the filter 301c, and also a predetermined amount of ink is stored.

On the internal lateral wall of the liquid chamber 301f, there is provided the liquid chamber groove structure 301j formed along the ink supply direction from the sub tank 301b to the liquid chamber 301f, namely along the vertical direction and extending from the bottom of the liquid chamber 301f to a position almost touching the filter 301c. The liquid chamber 301f has a substantially rectangular transversal cross section, and the aforementioned groove structure 301i is provided on both longitudinal ends in the cross section of the liquid chamber 301f. The groove structure 301j, to be explained later in more details, has such a dimension and a shape that the ink in the liquid chamber 301f

can be held by surface tension in the groove structure 301j and can thus be contacted with the lower surface of the filter 301c. Thus the ink in the liquid chamber 301f is connected with the ink in the sub tank 301b through the groove structure 301j and the filter 301c. Consequently, the minimum necessary ink amount to be accumulated in the liquid chamber 301f is an amount required for filling the nozzle 301g with ink, also for securing the gas of desired amount by the gas holding area formed by the liquid chamber 301f, filter 301c and groove structure 301j, and for connecting with the ink in the sub tank 301b through the groove structure 301j and the filter 301c. Also since the groove structure 301j holds the ink by the surface tension, the gas in the gas holding area cannot enter the groove structure 301j by breaking the surface tension of the ink.

Based on such configuration of providing the liquid chamber 301f with the groove structure 301j, contacting the upper surface of the filter 301c with the ink in the sub tank 301b, forming the gas holding area on the lower surface to hold the gas of the desired amount, and in an adjacent position contacting the ink with the filter 301c utilizing the groove structure 301j and the surface tension, the ink achieves connection through the filter 301c in a portion thereof in contact with the ink on the upper

and lower surfaces. The area of such ink connection in the filter 301c constitutes the effective area thereof. In the present embodiment, the groove structure 301j is provided in plural units on each of
5 the longitudinal ends of the liquid chamber 301f in the lateral cross section thereof, thereby increasing the effective area of the filter 301c and reducing the pressure loss therein.

In the above-described configuration, as the
10 ink in the liquid chamber 301f is consumed by the ink discharged from the nozzle 301g, the negative pressure in the liquid chamber 301f gradually increases. The ink in the liquid chamber 301f is connected with the ink in the sub tank 301b through
15 the groove structure 301j and the filter 301c, and the ink can easily move in such connecting portion. Therefore, when the negative pressure in the liquid chamber 301f increases, the ink in the sub tank 301b flows into the liquid chamber 301f through the
20 portion of the filter 301c where the lower surface is in contact with the ink, and through the groove structure 301j.

In case of a long standing in this state, gas is accumulated in the recording head 301 to induce
25 various drawbacks as in the first embodiment, but, against such gas accumulation, the present embodiment can maintain the ink discharging performance in

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stable manner over a long period, as in the first
embodiment, by filling the ink from the main tank 304
into the sub tank 302b and the liquid chamber 301f.
The ink filling from the main tank 304 into the sub
5 tank 301b and the liquid chamber 301f and the setting
of the volumes thereof are similar to those in the
first embodiment, but the ink filling condition and
the specific numbers of the respective volumes are
different from those in the first embodiment since,
10 in the present embodiment, the ink in the sub tank
301b is in contact with that in the liquid chamber
301f through the groove structure 301j and the filter
301c.

In the following there will be explained
15 specific examples of the aforementioned ink filling
operation into the sub tank 301b and the liquid
chamber 301f and of the volume setting.

It is assumed, as in the first embodiment, that
the ink filling is executed every month, and the gas
20 accumulating amount per month is 1 ml in the sub tank
301b and 0.5 ml in the liquid chamber 301f. It is
also assumed that the ink amount required in the sub
tank 301b not to expose the filter 301c to gas is 0.5
ml while the ink amount required in the liquid
25 chamber 301f not to expose the nozzle 301g to gas is
0.5ml, and the fluctuation in the ink filling amount
is 0.2 ml both in the sub tank 301b and the liquid

chamber 301f. Thus the ink amount to be filled in a single filling operation is the sum of these amounts, and is 1.7 ml in the sub tank 301b and 1.2 ml in the liquid chamber 301f. The suction pump 307c is
5 capable of pressure reduction to 0.8 atm (81.060 kPa).

The reduced pressure in the recording head 301 under these conditions is selected, within the power limit of the suction pump 307c, by the suction amount of the suction pump 307c so as to realize a pressure
10 of -0.6 atm (-60.795 kPa) in the suction cap 307a.

As the pressure required for gas permeation against the meniscus in the nozzle 301g is experimentally -0.05 atm (-5.06625 kPa), the pressure in the liquid chamber 301f becomes higher than that
15 in the suction cap 307a by 0.05 atm (5.06625kPa) as in the first embodiment. Similarly, as the pressure required for gas permeation against the meniscus in the filter 301 c is experimentally -0.1 atm (-10.1325 kPa), the pressure in the sub tank 301b becomes
20 higher than that in the liquid chamber 301f by 0.1 atm (10.1325 kPa). Therefore, by setting the pressure in the suction cap 307a at -0.6 atm (-60.795 kPa), the pressure in the liquid chamber 301f becomes -0.55 atm (-55.72875 kPa) while that in the sub tank
25 301b becomes -0.45 atm (-45.59625 kPa).

In order to fill the sub tank 301b with ink of 1.7 ml, the volume V1 thereof is so selected that the

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internal pressure becomes -0.45 atm (-45.59625 kPa) when ink of 1.7 ml is sucked from the sub tank 301b having an internal pressure of about 1 atm (101.325 kPa). Thus, $V1 = 1.7/0.45 = 3.78 \text{ ml}$. Similarly the
5 volume $V2$ of the liquid chamber 301f can be determined as $V2 = 1.2/0.55 = 2.18 \text{ ml}$.

After the internal pressure of the recording head 301 is reduced under the foregoing conditions, the shut-off valve 310 of the ink supply unit 305 is
10 opened whereby the ink flows into the recording head 301 in a reduced pressure state. More specifically, at first the ink flows into the sub tank 301b whereby the gas inflated to the volume $V1$ under reduced pressure is restored almost to the atmospheric
15 pressure. The gas volume $V1a$ in the sub tank 301b in such state is given by $V1a = V1 \times (1 - 0.45) = 2.08 \text{ ml}$, and the filling is terminated when ink in an amount of $V1 - V1a = 1.7 \text{ ml}$ is filled into the sub tank 301b. Similarly, in the liquid chamber 301f,
20 the ink flows from the sub tank 301b whereby the gas inflated to the volume $V2$ under reduced pressure is restored almost to the atmospheric pressure. The gas volume $V2a$ in the liquid chamber 301f in such state is given by $V2a = V2 \times (1 - 0.55) = 0.98 \text{ ml}$, and the
25 filling is terminated when ink in an amount of $V2 - V2a = 1.2 \text{ ml}$ is filled into the liquid chamber 301f.

Thus, by setting the volumes and reduced

pressures of the sub tank 301b and the liquid chamber 301f in the above-described manner, it is rendered possible to fill the sub tank 301b and the liquid chamber 301f, separated by the filter 301c, with the ink of appropriate amounts in a single filling operation, so that the recording head can be properly operated over a long period even in a situation where gas is accumulated therein.

Also, in the present embodiment, the effective area of the filter 301c remains substantially constant, because, on the lower surface of the filter 301c, there are substantially fixed the area holding the ink by surface tension in cooperation with the groove structure 301j and the area in contact with the gas of the gas holding area.

Therefore, the necessary effective area of the filter 301c can be controlled in consideration of the above-mentioned fact in the design stage, whereby, as in the first embodiment, there can be significantly improved the reliability against the discharge failure resulting from the bubble generation in the liquid chamber 301f or the movement of generated bubble.

The groove structure 301j in the present embodiment functions similarly to the partition portion 201e (cf. Fig. 5) in the first embodiment. More specifically, in case the ambient temperature

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rises while the shut-off valve 310 of the ink supply
unit 305 is closed to maintain the interior of the
recording head 301 in a closed system in which the
ink is held by the meniscus pressure at the surface
5 of the nozzle 301g, the groove structure 301j serves
to regulate the pressure increase resulting from the
gas inflation or the increase in the vapor pressure
in the liquid chamber 301f.

In case of gas inflation or an increase in the
10 vapor pressure in the liquid chamber 301f while the
recording head constitutes a closed system, the ink
in the liquid chamber 301f is pushed out to the
exterior by the gas volume corresponding to such
inflation or increase in the vapor pressure. As the
15 ink held by the groove structure 301j is in contact
with the filter 301c and the ink can easily pass
through the filter 301c in such contact portion,
there is realized a condition that the "force
required for breaking the meniscus formed in the
20 nozzle 301g" is equal to or larger than the "force
required for ink movement in the filter 301c",
whereby the ink in the liquid chamber 301f flows into
the sub tank 301b through the groove structure 301j
and the filter 301c. On the other hand, in the sub
25 tank 301b, as in the first embodiment, the gas
inflation or the increase in vapor pressure in the
sub tank 301b resulting from the ambient temperature

and the volume increase resulting from the ink flow from the liquid chamber 301f are absorbed by the pressure adjusting chamber 301i.

As explained in the foregoing, the groove structure 301j of the present embodiment allows to always maintain the ink in contact also with the surface of the filter 301c at the side of the liquid chamber 301f. Therefore, even in case of gas inflation or an increase in the vapor pressure in the liquid chamber 301f, the ink of an amount corresponding to the gas volume increase can be moved smoothly to the sub tank 301b through the filter 301c, thereby preventing the ink blow-out phenomenon from the nozzle 301g. Also the groove structure 301j is not particularly limited in number or position, but it is preferred to increase the number of the groove structure and to reduce the gap thereof in order to hold a larger amount of ink and to contact a larger amount of ink with the filter 301c.

The present embodiment shows a configuration where the liquid chamber 301f is provided with the groove structure 301j for contacting the ink with a part of the lower surface of the filter 301c, but such groove structure 301j may also be combined with the structure shown in the first embodiment. Fig. 12 is a cross-sectional view showing the internal structure of the recording head in such case.

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partition portion groove structure.

[Other embodiments]

In the following there will be explained the detailed structures applicable to the foregoing
5 embodiments.

(Positional relationship of filter and groove structure)

Fig. 13 is a lateral view showing the positional relationship between the groove structure
10 and the filter in the upper end portion of the groove structure. In Fig. 13, the filter 501c is supported at the periphery thereof, and a gap t is present between the filter 501c and the groove structure 501h. The groove structure 501h herein collectively means a
15 structure capable of holding the ink by the surface tension thereof and contacting it with the lower surface of the filter 501c, and more specifically indicates the plural ribs on the partition portion in the first embodiment, or the groove structure in the
20 liquid chamber or the plural ribs on the partition portion in the second embodiment. The term "groove structure" in the following description has the same meaning.

As indicated by a hatched area in Fig. 13, the
25 ink is held by the surface tension between the filter 501c and the groove structure 501h. An increase in the gap t between the filter 501c and the groove

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structure 501h reduces the surface tension, whereby
the ink holding state by the surface tension between
the filter 501c and the groove structure 501h can no
longer be maintained and becomes broken for example
5 by the weight of the ink itself or by vibration.

In the following there will be shown the result
of investigation by the present inventors on the
relationship of the gap t and the ink holding state
between the filter 501c and the groove structure 501h.

10 In this investigation, the recording head of
the foregoing embodiments was provided with a groove
structure 501h of a depth (lateral length thereof in
Fig. 13) of 2 mm and an aperture width (groove width)
of 0.5 mm, and ink of a surface tension of 35 mN/m
15 was filled according to the foregoing embodiments.
There was experimented the presence of ink leakage
from the nozzle when the temperature of the recording
head was changed from 5°C to 60°C. The obtained
results are shown in Table 1.

20

Table 1

Gap t (mm)	Head Still State	Head Driven State
0	No ink leakage	No ink leakage
0.5	No ink leakage	No ink leakage
0.8	No ink leakage	No ink leakage
1.0	Ink leakage from some nozzles	No ink leakage
1.2	Ink leakage from all nozzles	Ink leakage from some nozzles

In Table 1, the temperature rise in the "head still state" means the ambient temperature change around the recording head from 5°C to 60°C. On the other hand, in the temperature rise in the "head driven state", the ink jet recording apparatus mounted with the recording head was operated at 5°C and the recording head was brought to 60°C by temperature increase under ink discharge.

In the experiment, in the "head still state", the ink leakage started from $t = 1.0$ mm. On the other hand, in the "head driven state", the ink leakage did not occur at $t = 1.0$ mm, presumably because, in such state, the ink in the liquid chamber is consumed to generate an ink flowing force from the sub tank to the liquid chamber through the filter 501c, whereby the ink holding state between the

filter 501c and the groove structure 501h could be maintained.

Based on these results, the ink leakage does not occur, for the gap t between the filter 501c and the groove structure 501h, in a condition $0 \leq t \leq 1.0$ mm, preferably $0 \leq t \leq 0.8$ mm.

The filter can be jointed for example by fusion. Fig. 14A is a lateral view of the vicinity of the groove structure 501k prior to the jointing of the filter 501c by fusion. As shown in Fig. 14A, a support face 532 for the filter 501c is provided with fusion ribs 532a. The fusion jointing of the filter 501c can be achieved by placing the filter 501c on the fusion ribs 532 and pressing the 501c to the support face 532 with an unrepresented fusing hone thereby fusing and crushing the ribs 532a. Fig. 14B shows a state after fusion jointing of the filter 501c. In such fusion jointed state of the filter 501c, thereby may be generated a gap between the filter 501c and the groove structure 501k because of the remainder of the fusion ribs 532a or the deformation in the filter 501c, though depending on the fusing condition, shape of fusion ribs 532a and shape of the filter 501c. Particularly in case the distance between the filter 501c and the groove structure 501k is large, such gap changes by the surface irregularity of the filter 501c after the

fusion jointing. In order to minimize such gap
(within the aforementioned range of t), it is
possible, as shown in Fig. 14C, to cause the groove
structure 501k to protrude from the support face 532a
5 by about 0.1 mm toward the filter 501c, thereby
maintaining the filter 501c and the groove structure
501k always in contact.

The above-mentioned method for controlling the
gap between the filter 501c and the groove structure
10 501k is applicable not only in case of the fusion
jointing of the filter 501c but also in other
jointing methods. However, in case of jointing with
adhesive, attention is necessary in using adhesive of
a low viscosity since such adhesive may flow into the
15 groove structure 501k to deteriorate the function
thereof.

(Shape of groove structure)

The ink lifting force F by the surface tension
in the groove structure is given by:

20
$$F = L \times T \times \cos\theta$$

wherein T is the surface tension of ink, θ is the
contact angle of ink in the groove structure, and L
is the circumferential length of the ink contact area
in the groove structure.

25 The weight W of the lifted ink is given by:

$$W = S_i \times h_i \times \rho \times g$$

wherein h_i is the height of lifted ink, ρ is density

of ink, g is the acceleration of gravity and S_i is the cross section of the ink contact area in the groove structure.

Since $F = W$, there can be obtained a
5 relationship $L \times T \times \cos\theta = S_i \times h_i \times \rho \times g$ which can be deformed as

$$h_i = L/S_i \times (T \cos \theta / \rho g) \quad (1)$$

Consequently, for a height d of the groove structure, the ink held by the groove structure can reach the
10 upper end thereof by the surface tension by so selecting the groove structure as to satisfy a condition $d \leq h_i$, whereby the ink can be contacted with the lower surface of the filter.

Now let us consider a recessed groove structure
15 601k as shown in Fig. 15, having a height d , a depth e and an aperture width f and composed of two rectangular pillars 601n positioned in contact with a wall portion 601m. Applying the equation (1) to such structure, there can be obtained:

$$\begin{aligned} 20 \quad h_i &= (2e + f)/ef \times (T \cos \theta / \rho g) \\ &= (1/e + 2/f) \times (T \cos \theta / \rho g) \end{aligned} \quad (1)$$

On the other hand, let us consider a recessed groove structure 611k as shown in Fig. 16, having a height d , a depth e and an aperture width f and composed of two
25 rectangular pillars 611n in a position separated by a distance j from a wall portion 611m. Applying the equation (1) to such structure, there can be

obtained:

$$\begin{aligned} h_i &= (2e)/ef \times (T \cos \theta / \rho g) \\ &= 2/f \times (T \cos \theta / \rho g) \end{aligned} \quad (3)$$

Based on the foregoing, h_i is proportional to a
5 constant $A = L/S$ unless the contact angle of the ink
in the groove structure is varied.

Figs. 17 to 22 show variations in the shape of
the groove structure.

A groove structure 621k shown in Fig. 17 has a
10 groove shape of wedge-shaped cross section. A groove
structure 631k shown in Fig. 18 has a groove shape of
semi-oval cross section. A groove structure 641k
shown in Fig. 19 is cylindrical, of which hollow
portion serves to hold the ink by surface tension. A
15 groove structure 661k shown in Fig. 21 has a star-
shaped cross section, and a portion where ink contact
faces mutually cross at an acute angle serves to hold
the ink by the surface tension. The groove structure
661k having the star-shaped cross section can be
20 considered as a group of wedge-shaped groove
structures, and the depth e and the aperture width f
are defined in the recessed portion. Also Figs. 20
and 22 show groove structures 651k, 671k formed as a
component including plural holes (hollow portions) of
25 circular or star-shaped cross section. A structure
for contacting the ink with the lower surface of the
filter can also be formed by placing a component as

shown in Fig. 20 or 22 immediately under the filter.
In the foregoing there have been explained various
forms of the groove structure, and the shape, number,
installing position and combination of such groove
5 structure can be arbitrarily changed within a range
not departing from the scope of the present invention.

Table 2 shows the ink lifting height h_i
(maximum height of groove structure) in some of the
aforementioned variations, with a depth $e = 2$ mm, in
10 which the constant A and the aperture width f is
changed from 0.3 mm to 2.0 mm by every 0.2 mm.

Table 2

Shape of groove structure	A (m^{-1})	Aperture width f (mm)								
		0.3	0.5	0.8	1.0	1.2	1.4	1.6	1.8	2.0
Wedge type	5099	40	24	15	12	10	9	8	7	7
Semi-oval type	3808	29	17	11	9	8	7	7	6	6
Recessed type	3000	21	13	9	7	6	6	5	5	4
Rectangular pillar type	1000	20	12	7	6	5	4	4	3	3

In the groove structure of "rectangular pillar
type", the value A is determined for an aperture
width $b = 1.6$ mm. Also in the "semi-oval type", the
depth e is defined as a half of the longer diameter

and the aperture width f is defined as the shorter diameter.

Fig. 23 is a chart showing the relationship between the aperture width f and the ink lifting height h_i . Referring to Fig. 23, in the "rectangular pillar type", the ink lifting height h_i is 3mm for $f = 2.0$ mm and 4 mm for $f = 1.6$ mm. The value $h_i = 3$ mm corresponds to a gas thickness at least required in the gas holding area under the filter. Also in consideration of the dimensional fluctuation in the components, there is required $h_i = 4$ mm. The constant A in such state is $A = 1250 \text{ m}^{-1}$. As indicated by the equation (3), the depth of the groove structure of "rectangular pillar type" does not influence the ink lifting height, so that the constant A of such structure can be considered as the lower limit of that in other groove structures influenced by the depth. Thus, if the gas in the gas holding area is thicker, there can be employed the groove structure of "wedge" or "recessed" type with a small aperture width f . Therefore, in order to realize the present invention, the constant A is preferably at least equal to 1000 m^{-1} , more preferably at least equal to 1250 m^{-1} .

A small bubble, if trapped in a corner portion of the groove structure, hinder the ink movement in the groove structure. In order to avoid such bubble

trapping, the ink moving portion of the groove structure and the vicinity thereof is preferably cut off or rounded at the edge. Also the corner portion of the filter is preferably cut off or rounded in order to prevent bubble trapping in such portion.

(Liquid chamber cover)

As shown in Fig. 10, a lateral face of the liquid chamber 301f may be composed of a cover member 701 separate from other portions. In the example shown in Fig. 10, the cover member 701 constitutes a face where the groove structure 301j is provided. Fig. 24 is a perspective view of such cover member 701.

As shown in Fig. 24, the liquid chamber cover 701 is provided, on a face thereof constituting the internal wall of the liquid chamber 301f (cf. Fig. 10), with grooves structures 710 having vertical slits 711 in protruding manner and in a number corresponding to the number of the liquid chambers 301f. Thus, in a state where the liquid chamber cover 701 is jointed to the main body 720 (cf. Fig. 10) constituting the main part of the liquid chamber 301f, the groove structures 710 are positioned in the respectively corresponding liquid chambers 301f. The vertical slit 711 serves as a structure for holding the ink in the liquid chamber 301f by the surface tension. Also at the base portion of each groove

by forming lateral slit 712 at the base portion of
the groove structure 710, the flowing adhesive can be
retained in such lateral slit 712 whereby more
effectively reducing the movement of the adhesive to
5 the vertical slit 711.

In the foregoing, the present invention has
been explained by preferred embodiments thereof, but
the present invention is not limited to such
embodiments and is applicable to various liquid
10 supply systems adapted to hold liquid in the negative
pressure state and including the liquid supply path
having a filter therein.

Also in the application of such liquid supply
system to the ink jet recording apparatus, the ink
15 supply system to the recording head is not limited to
the tube supply system explained in the foregoing
embodiments but can also be the pin-in system, with
similar effects. It is also applicable to the
recording head of head tank integral system, by using
20 the sub tank as the main ink tank. In such case, the
recording head of head tank integral type itself is
constituted as the ink supply system. More
specifically, the sub tank is provided with an air
communicating aperture to be opened or closed by an
25 unrepresented valve mechanism, and, at the ink
filling into the liquid chamber, such air
communicating aperture is closed and the interior of

the recording head is reduced to a desired pressure
by the suction from the nozzle, and then the air
communicating aperture is opened, whereby an
appropriate amount of ink is supplied into the liquid
5 chamber.

Also in the foregoing embodiments, there have
been explained the ink jet recording apparatus of
serial scan type, but the present invention is
likewise applicable to an ink jet recording apparatus
10 mounted with an ink jet recording head of line type,
having the nozzle array over the entire width of the
recording medium.

As explained in the foregoing, the present
invention provides the configuration in which the
15 filter and the liquid are separated by gas of the gas
holding area at the downstream side of the filter,
thereby avoiding the drawback, in case the bubble is
generated at the downstream side of the filter, in
the liquid supply from the upstream side of the
20 filter to the downstream side thereof, induced by
such bubble. Particularly in the ink jet recording
head and in the ink jet recording apparatus, it is
rendered possible to prevent defective ink discharge
resulting from the deficient ink supply to the
25 downstream side of the filter, thereby significantly
improving the reliability on the ink discharge. Also
at the downstream side of the side, there is provided

a structure for holding the liquid, present at the downstream side of the film across the gas of the gas holding area, by the surface tension for connecting such liquid with the liquid at the upstream side of the filter, or a liquid chamber for so holding the liquid as to contact it with a part of the downstream face of the filter, whereby the liquid held in the downstream side of the filter can escape to the upstream side through the filter in case of inflation of the gas in the gas holding area, so that the unexpected liquid flow-out from the downstream end of the liquid supply path or from the discharge portion in case of the ink jet recording head.

Also the liquid filling method of the present invention allows to fill the first and second liquid chambers with the liquid of respectively appropriate amounts even in case the liquid amounts therein decrease by the gas accumulation therein.